PRESENTATION OUTLINE

• Introduction
• Materials and methods
• RSW parameter optimization
• Microstructure and micro-hardness characterization
• KS-II combined loading results
• Conclusions
INTRODUCTION TO 3RD GEN AHSS

First generation AHSS: lean compositions, better strength and crash performance than HSS.
Second generation AHSS: Superior mechanical properties, elevated alloying additions, relatively expensive.
Third generation AHSS: Better strength/ductility than 1G AHSS, lower allowing elements than 2G AHSS.

High strength to weight ratio of 3G-AHSS

- Weight reduction
- Reduced greenhouse emissions
- Better fuel efficiency
- Improved crash properties

1WordAutoSteel. Advanced high strength steel (AHSS) application guidelines (version 4.1). WorldAutoSteel; June 2009.
INTRODUCTION TO RSW PROCESS

Resistance Spot Welding is the most common joining technique in the automotive industry

2000-6000 Spot Welds in a typical BIW

(I) Initial configuration  (II) Squeezing  (III) Welding  (IV) Cooling  (V) Unclamping
OBJECTIVE

Characterize mechanical performance and failure behavior of 3rd Gen AHSS spot welded joints upon combined loading condition

• Load bearing capacities
• Energy absorption capabilities
• Failure response
MATERIALS AND METHODS

Material | Carbon equivalent | Nominal sheet thickness [mm] | YS [MPa] | UTS [MPa] | El [%]
--- | --- | --- | --- | --- | ---
3G-980 (uncoated) | 0.64 | 1.4 | 616±2.64 | 1013±15.4 | 19.89
3G-1180 (uncoated) | 0.7 | 1.4 | 967±7.05 | 1181±19.0 | 11.83

YS, yield strength; UTS, ultimate tensile strength; TE, total elongation; UE, uniform elongation;

Welding schedule was selected based on recommendation of AWS D8.9 standard.

Honda RSW Robot

<table>
<thead>
<tr>
<th>Material</th>
<th>Number of pulses</th>
<th>Total welding time (ms)</th>
<th>Squeeze time (ms)</th>
<th>Hold time (ms)</th>
<th>Cooling between pulses (ms)</th>
</tr>
</thead>
<tbody>
<tr>
<td>3G-980 (uncoated)</td>
<td>2</td>
<td>334</td>
<td>167</td>
<td>167</td>
<td>34</td>
</tr>
<tr>
<td>3G-1180 (uncoated)</td>
<td>2</td>
<td>334</td>
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<td>167</td>
<td>34</td>
</tr>
</tbody>
</table>
MATERIALS AND METHODS

KS-II combined loading mechanical testing methodology:

Tests were coupled with three dimensional Digital Image Correlation (DIC)
OPTIMIZED RSW PARAMETERS

Welding current parameter was optimized by performing traditional Lap Shear and Cross Tension mechanical tests at 0.5 kA welding current intervals and selecting the highest load bearing capability without expulsion.

Minimum weld size of $4\sqrt{t} = 4.7$ mm

Electrode face diameter weld size of 7mm
OPTIMIZED RSW CHARACTERISTICS

The optimized welding schedule resulted in a face diameter weld size (FDWS) of 7 mm for both materials.

Average FZ hardness of 490 HV
Min hardness in SCHAZ 340 HV
Average BM hardness of 380 HV

Average FZ hardness of 540 HV
No HAZ softening
Average BM hardness of 300 HV
KS-II MECHANICAL TEST RESULTS

Noticeable slippage and rotation of specimen at shear-dominated loading orientations

Negligible slippage and rotation of specimen at tensile-dominated loading orientations
KS-II MECHANICAL TEST RESULTS

Snapshots of different loading orientations showing a combination of rotation and slippage at shear-dominated loading orientations.
KS-II MECHANICAL TEST RESULTS

Novel local nugget displacement methodology proposed to minimize influence of coupon rotation and slippage on spot weld performance indices.
KS-II MECHANICAL TEST RESULTS

First benefit of local nugget displacement: more accurate calibration of force-based failure criterion

Tensile component [kN]
Shear component [kN]

Nominal Orientation Fit

3G-980
3G-1180

75° 60° 45° 30° 15° 10°

Final Orientation Fit

3G-980
3G-1180

75° 60° 45° 30° 15° 10°

Considering final orientation of the nugget

Instead of nominal orientation at the beginning of the tests
KS-II MECHANICAL TEST RESULTS

Second benefit of local nugget displacement: Capability to calculate spot weld energy absorption capability in shear and tensile directions independently.

Absorbed energy [J] vs Loading orientation (θ)

3rd Gen -980

3rd Gen -1180

IF P-PO PO

IF P-PO
Failure analysis: Interrupted KS-II tests within shear-dominated loading orientations revealed tendency of failure through softened SCHAZ for 3rd Gen-1180 joints.
KS-II MECHANICAL TEST RESULTS

- Failure analysis: Interrupted KS-II tests within tensile-dominated loading orientations revealed tendency of crack propagation within the fusion zone of 3rd Gen-1180.
- Propagation of cracks into the fusion zone of 3rd Gen-1180 spot welds is causing limited post-failure energy absorption.
SUMMARY

• RSW process was optimized for investigated 3rd Gen AHSS by producing joints with optimum load bearing capacities during lap shear and cross tension tests.

• Mechanical properties (strength and energy absorption) and failure characteristics of 3rd Gen AHSS spot welds under combined loading conditions were investigated.

CONCLUSIONS

• A novel methodology coupling digital image correlation with KS-II testing was proposed.

The proposed methodology allows for:
• more accurate calibration of strength-based failure criteria
• instantaneous quantification of nugget orientation
• more precise measurement of nugget displacement
• minimizing the influence of slippage and deformation
• increased accuracy for spot weld energy absorption calculation
• Calculating in shear and tensile directions separately

• Propagation of the cracks into the fusion zone of the 3rd Gen-1180 spot welds is responsible for their inferior energy absorption and strength compared to 3rd Gen-980 spot welds within tensile-dominated loading orientations.
More Questions? Meet the speaker at the Auto/Steel Partnership booth after this presentation.
KS-II MECHANICAL TEST RESULTS

Second benefit of local nugget displacement: Capability to calculate spot weld energy absorption capability in shear and tensile directions independently.

Acquire load- crosshead displacement curve
Calculate projected nugget displacement ($d$) vector
Decompose load and displacement vectors to shear and tensile components
Calculate energy dissipation due to $\delta s$, $\delta t$, and $d$ displacements separately

Energy dissipation due to $\delta s$

\[ E_{\delta s} = w_1 \]
\[ E_{ap} = w_2 \]
\[ E_{\delta s} = w_1 + w_2 \]

Energy dissipation due to $\delta t$

\[ E_{\delta t} = w_3 \]
\[ E_{ap} = w_4 \]
\[ E_{\delta t} = w_3 + w_4 \]

Energy dissipation due to $d$

\[ E_{up} = w_1 + w_3 \]
\[ E_{ap} = w_2 + w_4 \]
\[ E_{total} = w_1 + w_2 + w_3 + w_4 \]
KS-II MECHANICAL TEST RESULTS

Third benefit of local nugget displacement: Exclusion of the influence of slippage and deformation at regions away from the spot weld on extracted load-displacement curves.

Crosshead displacement

CO point displacement

Nugget displacement

3G-980 KS-II 0° vs Lap Shear

3G-1180 KS-II 0° vs Lap Shear

3G-980 KS-II 90° vs Cross Tension

3G-1180 KS-II 90° vs Cross Tension

Interfacial failure with limited deformation
Pullout with severe rotation and deformation

Noticeable plastic deformation around the nugget